

BSIM4v4.7.0

Enhancements and Bug Fixes

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BSIM4v4.7.0 Bug-fix

Code inconsistency in files b4set.c and b4ld.c:

File b4set.c Line: 208

```
if (!model->BSIM4toxmgiven)
    model->BSIM4toxm = model->BSIM4toxe;
```

File b4temp.c Line: 134

```
else if ((!model->BSIM4toxeGiven) && (model->BSIM4toxpGiven))
{
    model->BSIM4toxe = model->BSIM4toxp + model->
BSIM4dtox;
if (!model->BSIM4toxmgiven)
    model->BSIM4toxm = model->BSIM4toxe; }
```

Reported by WENLI WANG, CADENCE

BSIM4v4.7.0 Bug-Fix

- **Source and Drain diode current shows unphysical and high values for $A_{\text{seff}}=P_{\text{seff}}=A_{\text{deff}}=P_{\text{deff}}=0$, although it shows correct prediction for positive values of A_{seff} , P_{seff} , A_{deff} and P_{deff} .**
- **Action:**
 - **If A_{seff} , P_{seff} , A_{deff} , P_{deff} are negative, their values are set to '0' .**
 - **For $A_{\text{seff}} \&\& P_{\text{seff}} = 0$, source side diode is turned off by setting `SourceSaturationCurrent=0.0`**
 - **For $A_{\text{deff}} \&\& P_{\text{deff}} = 0$, drain side diode is turned off by setting `DrainSaturationCurrent=0.0`**

(Code with red font is replaced by that with blue.)

Reported by Jushan Xie, CADENCE

Bug-fix Assistance: Jushan Xie, Samuel Mertens (ANSOFT)

BSIM4v4.7.0 Bug-Fix

```
if (here->BSIM4sourcePerimeterGiven)
```

[Source side]

```
{ if (model->BSIM4perMod == 0)
```

```
here->BSIM4Pseff = here->BSIM4sourcePerimeter;
```

```
else
```

```
here->BSIM4Pseff = here->BSIM4sourcePerimeter
```

```
- pParam->BSIM4weffCJ * here->BSIM4nf;
```

```
} b4temp.c (1742-1748)
```

```
if (here->BSIM4sourcePerimeterGiven)
```

[Source side]

```
{ if (here->BSIM4sourcePerimeter == 0.0)
```

```
here->BSIM4Pseff = 0.0;
```

```
else if (here->BSIM4sourcePerimeter < 0.0)
```

```
{ printf("Warning: Source Perimeter is specified as negative, it is set to zero.\n");
```

```
here->BSIM4Pseff = 0.0;}
```

```
else
```

```
{ if (model->BSIM4perMod == 0)
```

```
here->BSIM4Pseff = here->BSIM4sourcePerimeter;
```

```
Else
```

```
here->BSIM4Pseff = here->BSIM4sourcePerimeter - pParam->BSIM4weffCJ * here->BSIM4nf;
```

```
}
```

```
}
```

BSIM4v4.7.0 Bug-Fix

```
if (here->BSIM4drainPerimeterGiven)
```

[Drain side]

```
{ if (model->BSIM4perMod == 0)
```

```
here->BSIM4Pdeff = here->BSIM4drainPerimeter;
```

```
else
```

```
here->BSIM4Pdeff = here->BSIM4drainPerimeter
```

```
-pParam->BSIM4weffCJ * here->BSIM4nf;
```

```
} b4temp.c (1758-1763)
```

```
if (here->BSIM4drainPerimeterGiven)
```

[Drainside]

```
{ if (here->BSIM4drainPerimeter == 0.0)
```

```
here->BSIM4Pdeff = 0.0;
```

```
else if (here->BSIM4drainPerimeter < 0.0)
```

```
{ printf("Warning: Drain Perimeter is specified as negative, it is set to zero.\n");
```

```
here->BSIM4Pdeff = 0.0;}
```

```
else
```

```
{ if (model->BSIM4perMod == 0)
```

```
here->BSIM4Pdeff = here->BSIM4drainPerimeter;
```

```
Else
```

```
here->BSIM4Pdeff = here->BSIM4drainPerimeter - pParam->BSIM4weffCJ * here->BSIM4nf;
```

```
}
```

```
}
```

BSIM4v4.7.0 Bug-Fix

```
if ((here->BSIM4Aseff <= 0.0) && (here->BSIM4Pseff <= 0.0)) [Source side]
    { SourceSatCurrent = 1.0e-14;
      }          b4ld.c (664-666), b4temp.c (1854-1856)
```

```
if ((here->BSIM4Aseff <= 0.0) && (here->BSIM4Pseff <= 0.0)) [Source side]
    { SourceSatCurrent = 0.0;
      }
```

```
if ((here->BSIM4Adeff <= 0.0) && (here->BSIM4Pdeff <= 0.0)) [Drain side]
    { DrainSatCurrent = 1.0e-14;
      }          b4ld.c (762-764), b4temp.c (1912-1914)
```

```
if ((here->BSIM4Adeff <= 0.0) && (here->BSIM4Pdeff <= 0.0)) [Drain side]
    { DrainSatCurrent = 0.0;
      }
```

BSIM4v4.7.0 Bug-Fix

if (here->BSIM4Aseff < 0.0)

here->BSIM4Aseff = 0.0;

b4temp.c (1778)

if (here->BSIM4Adeff < 0.0)

here->BSIM4Adeff = 0.0;

b4temp.c (1785)

BSIM4v4.7.0 Bug-Fix

Redundant 'toxe' term appearing in the Igc formulation:

BSIM 4.6.4 users manual Equ 4.6.1

$$PIGCD = \frac{B \cdot TOXE}{V_{gsteff}^2} \left(1 - \frac{V_{dseff}}{2 \cdot V_{gsteff}} \right)$$

Code implementation:

```
pParam->BSIM4Bechvb = (model->BSIM4type == NMOS) ? 7.45669e11 :  
1.16645e12; b4temp.c (1276)
```

```
pParam->BSIM4Bechvb *= -toxe; b4temp.c (1285)
```

```
T11 = pParam->BSIM4Bechvb * toxe; b4ld.c (2387)
```

Fix: T11 = -pParam->BSIM4Bechvb

Reported by Kyoon-Hyoung Kim, Hynix Semiconductor

BSIM4v4.7.0 Enhancements

Requested by

**Wenwei Yang and Jung-Suk Goo
Globalfoundries**

Enhancement of GIDL/GISL Model

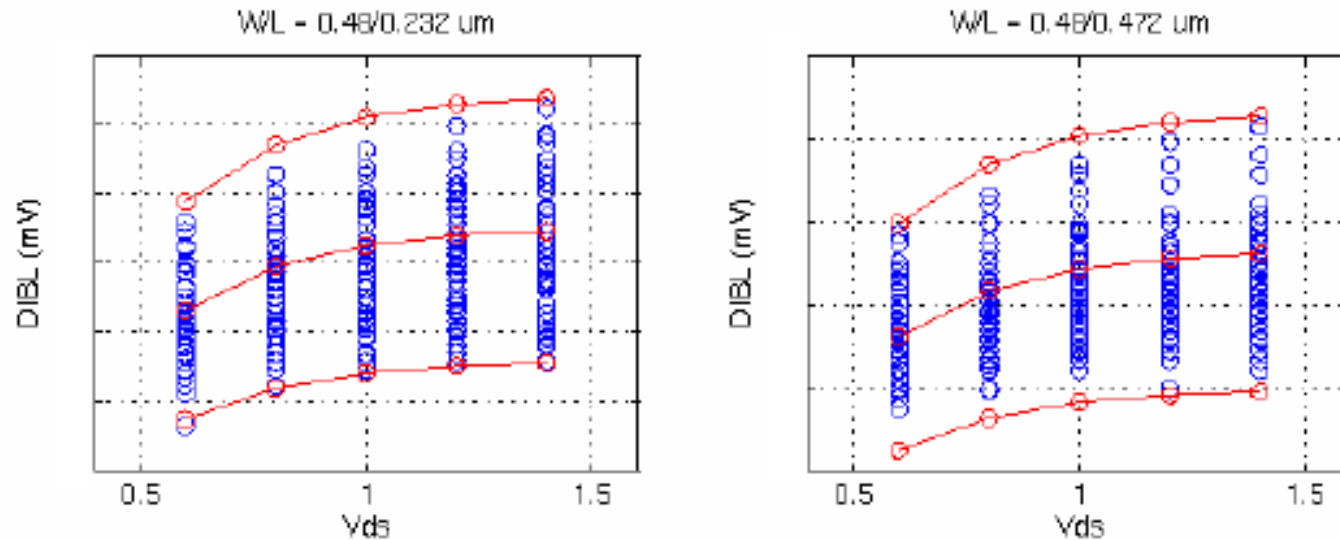
- **GIDLMOD=1** is introduced to decouple V_d from V_g through new parameters **RGIDL**, **KGIDL** and **FGIDL** (same for **GISL**)

$$I_{GIDL} = A_{GIDL} W_{diod} \cdot N_f \cdot \frac{V_{ds} - RGIDL V_{gse} - EGIDL + V_{fbsd}}{3 \cdot T_{oxe}} \cdot \exp\left(-\frac{3 \cdot T_{oxe} \cdot BGIDL}{V_{ds} - V_{gse} - EGIDL}\right) \cdot \exp\left(\frac{KGIDL}{V_{ds} - FGIDL}\right)$$

- **Status:**
 - Binnable parameters **RGIDL**, **KGIDL**, **FGIDL** introduced with new Mod selector, `gidlMod=1`
 - Backward compatible

Enhancement of DIBL/Rout Model

- Existing DIBL /Rout model in BSIMSOI is proposed to enhance with additional term DVTP5, to better capture Vds effect in long channel device



- Current formulation cannot capture this asymmetric variation

Enhancement of DIBL/Rout Model

- The $\tanh()$ function enables capturing the effect
- **Proposal: Implement the enhanced model in BSIM4**

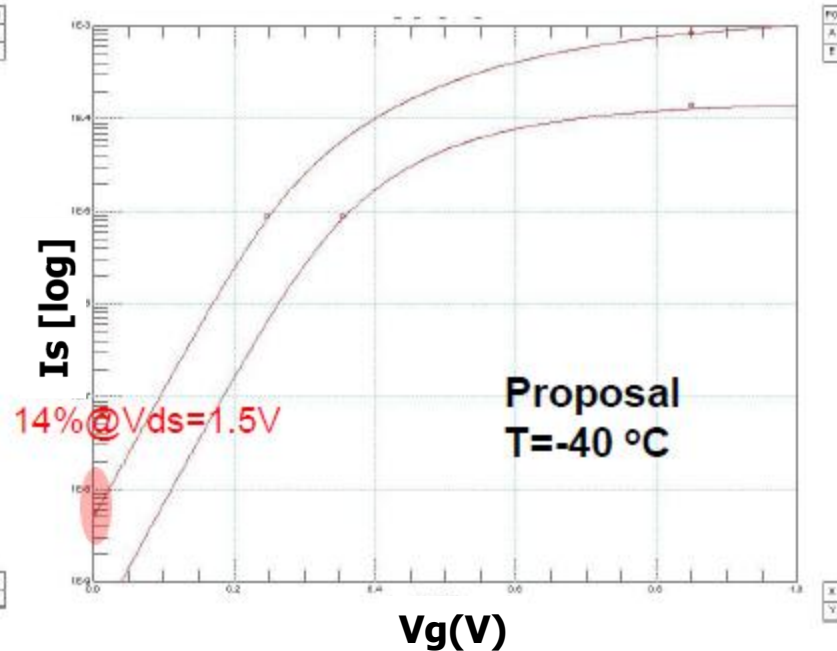
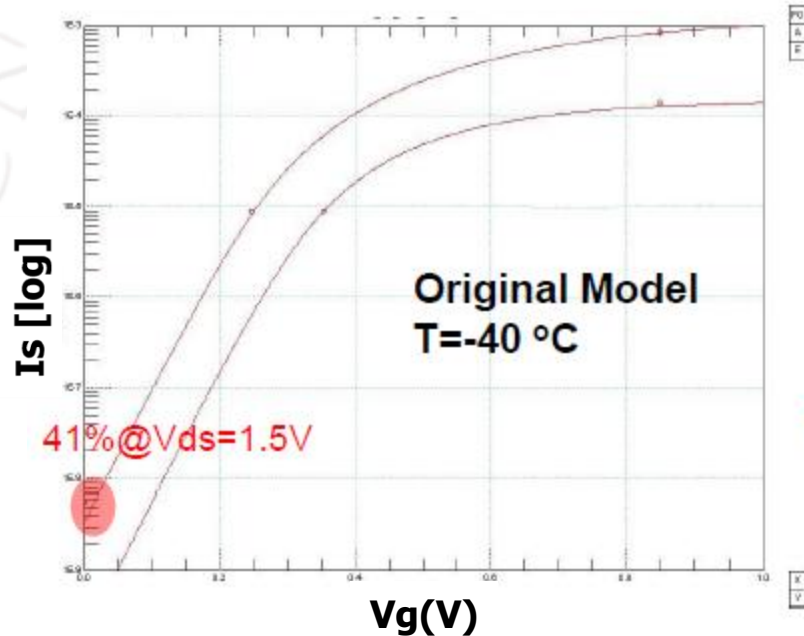
$$V_{th} = V_{th0} + \dots - \left(DVTP5 + \frac{DVTP2}{L_{eff}^{DVTP3}} \right) \cdot \tanh(DVTP4 \cdot V_{ds})$$

New term for BSIM4

- **Enhancements:**
- **Proposed model implemented with Binnable parameters DVTP2, DVTP3, DVTP4, DVTP5**
- **Backward compatible**

Temperature Dependence of Sub-threshold Leakage Current

- Improved formulations are suggested (reviewed by IBM) to capture temperature dependence of Leakage Current:



$$\text{Error} = (\text{Model} - \text{Si}) / \text{Si}$$

Temperature Dependence of Subthreshold Leakage Current

■ Suggested equations:

- $N_{\text{factor}}(T) = n_{\text{factor}}(T_{\text{nom}}) + \text{tnfactor} * (T/T_{\text{nom}} - 1)$
- $\text{ETA0}(T) = \text{ETA0}(T_{\text{nom}}) + \text{TETA0} * (T/T_{\text{nom}} - 1)$
- $\text{voffCV}(T) = \text{voffCV} * (1.0 + \text{tvoffCV} * (T - T_{\text{nom}}))$

■ Enhancements

- Suggested temperature dependence model has been implemented with new Binnable parameters (Red fonts)
- Backward Compatible

CODE MODIFICATIONS

- List of code modification:**

Enhancements/ Bug-Fix	REPORTED BY	File	Line(s)
Code inconsistency	Wenli Wang, CADENCE	b4temp.c	134
Diode 'off' current	Jushan Xie, CADENCE	b4ld.c, b4temp.c	664, 762 1742,1758,1778,1785, 1854,1913
Igc formulation	Kyoon-Hyoung Kim HYNIX SEMI	b4ld.c	2387
New GIDL/GIDL	Wenwei Yang, Jung-Suk Goo GLOBAL- FOUNDRIES	b4.c, b4ld.c, b4mask.c, b4mpar.c, b4set.c, b4temp.c, bsim4def.h	Various locations
New DIBL/Rout			
Temp. Dependence of sub-threshold current			

Diode Ideality Factor

- Limit the minimum value of diode ideality factors N_{JD} and N_{JS}
 - Warning when these values are below 0.7.
 - Limit the minimum value to 0.1.

MOD Switch for mtrlMod=0,1 Compatibility

- New materials MOD (mtrlMod):
 - mtrlMod=0 and mtrlMod=1 behaves differently even with EOT=TOXE and EPSROX=3.9.
 - Reported by Wenwei Yang (GlobalFoundries)
 - **“mtrlCompatMod” added to make the two consistent**

Investigation and Fixing of mtrlMod=0,1 Discrepancy

- Physical oxide thickness calculation

T_{oxp} is a complex function of EOT for mtrlMod=1

$T_{\text{oxp}} = \text{TOXE} - \text{D TOX}$ for mtrlMod=0

Fix: New MOD switch mtrlCompatMod introduced

$T_{\text{oxp}} = \text{EOT} * \text{EPSROX} / 3.9 - \text{D TOX}$ when mtrlCompatMod=1 and mtrlMod=1

- Effective field for mobility calculation

$E_{\text{eff}} (V_{\text{gsteff}} + 2V_{\text{th}} - 2(V_{\text{fb}} + \Phi_{\text{st}}))$ for mtrlMod=1

$E_{\text{eff}} (V_{\text{gsteff}} + 2V_{\text{th}})$ for mtrlMod=0

Fig: $2(V_{\text{fb}} + \Phi_{\text{st}})$ is dropped when mtrlCompatMod=1

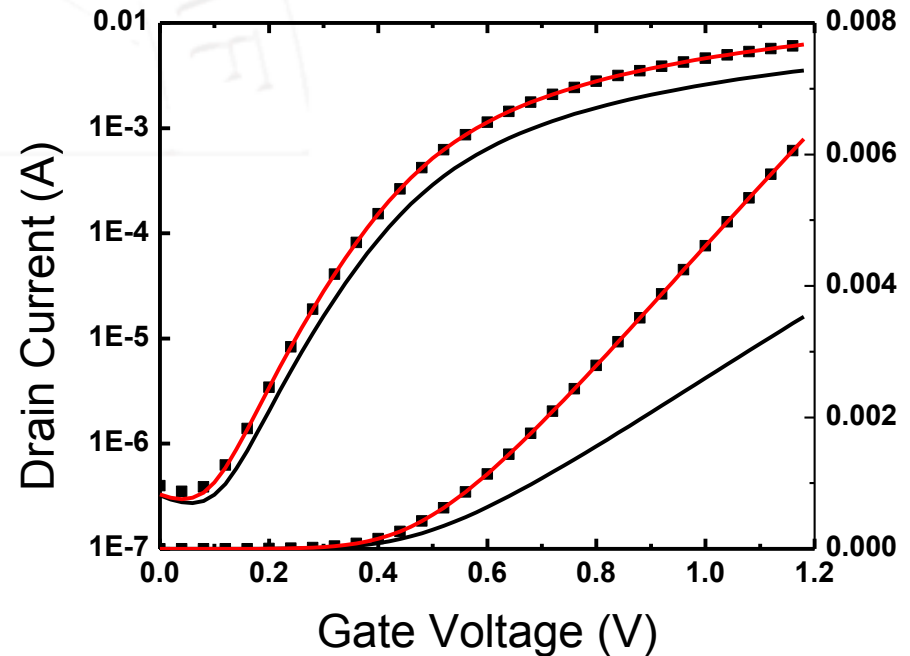
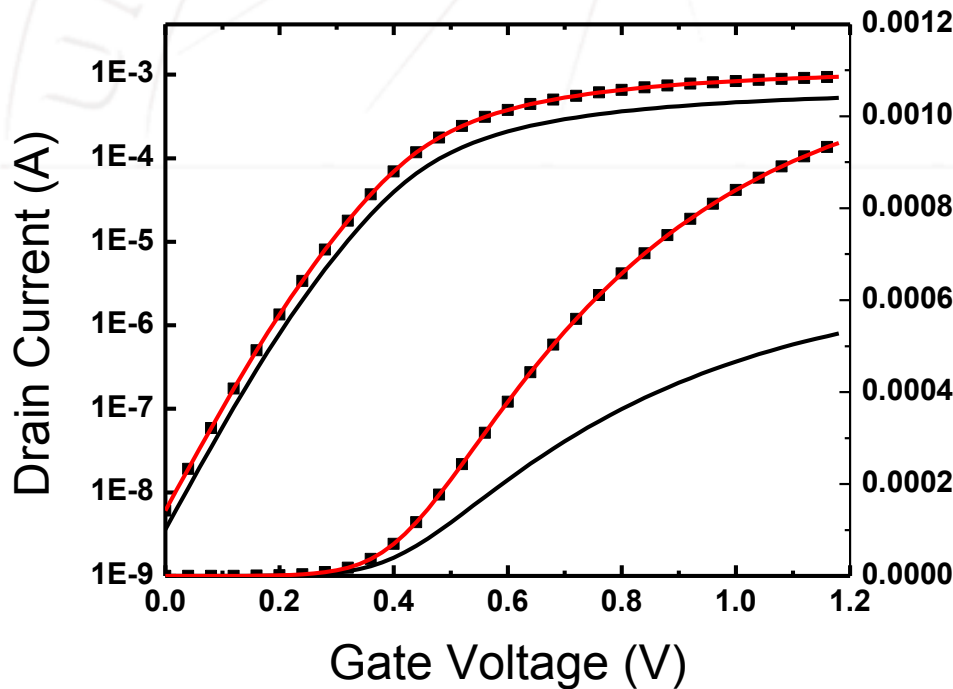
Ref: C. Hu, "MOS Transistor," in Modern Semiconductor Devices for Integrated Circuits. Prentice Hall, 2009, ch. 6.

New switch “mtrlCompatMod” introduced to make mtrlMod=0 compatible with mtrlMod=1

- Symbols: mtrlMod=0
- Lines: — mtrlMod=1; mtrlCompatMod=0
— mtrlMod=1; mtrlCompatMod=1 (BSIM v4.7)

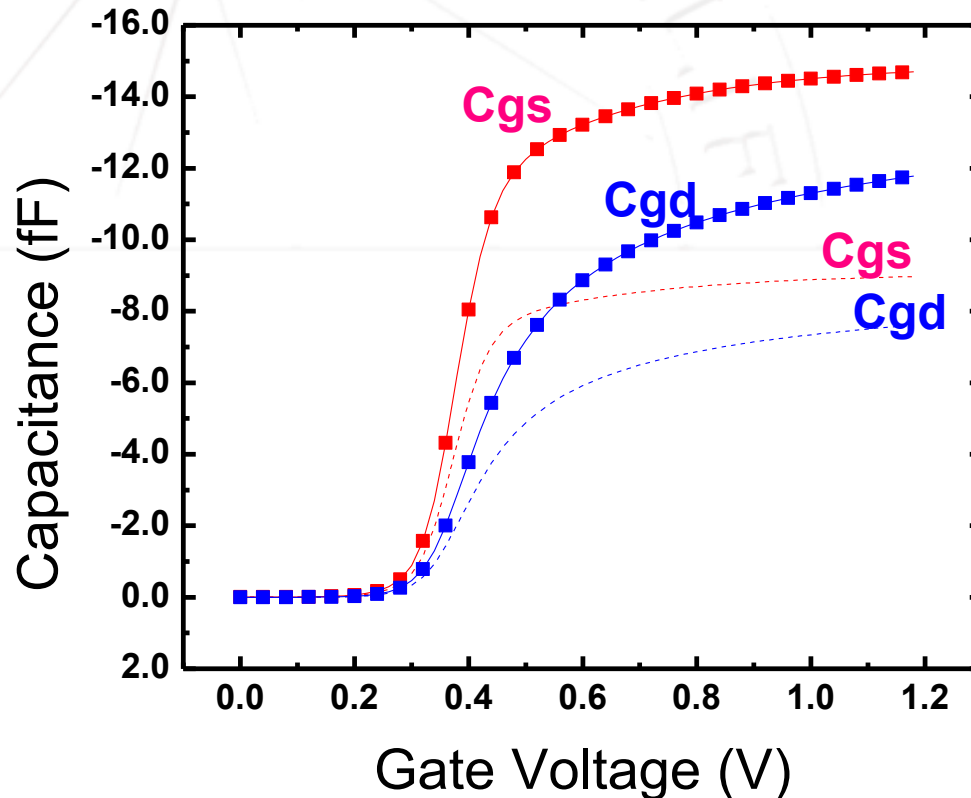
Idlin

Idsat



C-V Discrepancy Also Fixed

- Symbols: mtrlMod=0
- Dashed Lines: mtrlMod=1; mtrlCompatMod=0
- **Solid Lines:** mtrlMod=1; mtrlCompatMod=1 (BSIM4.7)



Enhanced Thermal Noise Model for BSIM4

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tnoiMod=2 implemented in SPICE3

- New expressions for drain noise (S_{id}), induced gate noise (S_{ig}) and correlation coefficient (c):

$$S_{id} = 4kT \cdot \gamma \cdot g_{d0} \cdot (3 \cdot \beta_{tnoi}^2)$$

$$S_{ig0} = 4kT \cdot C_0^2 \cdot \omega^2 \cdot \frac{\delta}{g_{d0}} \cdot \left(\frac{15 \cdot \theta_{tnoi}^2}{4} \right)$$

$$c = -j \frac{\epsilon}{\sqrt{\gamma \cdot \delta}} \cdot \left(\frac{c_{tnoi}}{0.395} \right)$$

$$g_{d0} = NF \times \frac{\mu_{eff} C_{oxeff} \frac{W_{eff}}{L_{eff}} V_{gsteff}}{1 + g_{che} \cdot R_{ds}}$$

$$C_0 = NF \times C_{oxeff} W_{eff,CV} L_{eff,CV}$$

$$\beta_{tnoi} = RNOIA \cdot \left[1 + TNOIA \cdot L_{eff} \cdot \left(\frac{V_{gsteff}}{E_{sat} L_{eff}} \right)^2 \right]$$

$$\theta_{tnoi} = RNOIB \cdot \left[1 + TNOIB \cdot L_{eff} \cdot \left(\frac{V_{gsteff}}{E_{sat} L_{eff}} \right)^2 \right]$$

$$c_{tnoi} = RNOIC \cdot \left[1 + TNOIC \cdot L_{eff} \cdot \left(\frac{V_{gsteff}}{E_{sat} L_{eff}} \right)^2 \right]$$

Default:

RNOIA=0.577

RNOIB=0.5164

RNOIC=0.395

Expressions for γ , δ and ϵ

$$\gamma = \frac{L}{L_{vsat}} \left[\frac{1 + \eta}{2} + \frac{(1 - \eta)^2}{6 \left[(1 + \eta) + \frac{2V_t \alpha}{V_{gsteff}} \right]} \right]$$

$$\delta = \frac{1}{6} \left(\frac{L_{vsat}}{L} \right)^3 \left[\frac{1 + \eta}{\left[(1 + \eta) + \frac{2\alpha V_t}{V_{gsteff}} \right]^2} - \frac{\left[6(1 + \eta) + \frac{2\alpha V_t}{V_{gsteff}} \right] (1 - \eta)^2}{15 \left[(1 + \eta) + \frac{2\alpha V_t}{V_{gsteff}} \right]^4} + \frac{(1 - \eta)^4}{9 \left[(1 + \eta) + \frac{2\alpha V_t}{V_{gsteff}} \right]^5} \right]$$

$$\epsilon = \frac{1}{6} \cdot \frac{L_{vsat}}{L} \left[\frac{1 - \eta}{\left[(1 + \eta) + \frac{2\alpha V_t}{V_{gsteff}} \right]} + \frac{(1 - \eta)^3}{3 \left[(1 + \eta) + \frac{2\alpha V_t}{V_{gsteff}} \right]^3} \right]$$

$$\alpha = A_{bulk}$$

$$\eta = 1 - \frac{V_{dseff}}{V_b}$$

$$L_{vsat} = L_{eff} \cdot \left[1 + \frac{V_{dseff}}{E_{sat} L_{eff}} \right]$$

$$V_b = \frac{V_{gsteff} + 2v_t}{A_{bulk}}$$

Summary of Code Changes

File	Line # (approx.)	Description
b4.c	1025	Entries for new parameters TNOIC, RNOIC added
b4mask.c	630	
b4mpar.c	870	
b4set.c	144	
b4check.c	719	Parameter checking for TNOIA, TNOIB, RNOIA and RNOIB are extended to tnoiMod=2,3
b4ld.c	1727	Definition of here->BSIM4Coxeff
	2890	Calculation of here->BSIM4noiGd0
b4noi.c	127	Definition of new noise source ".corl"
	248	Calculation of Rs,Rd noise for tnoiMod=2,3
	390	Noise calculation for tnoiMod=2,3
bsim4def.h	164,440,977,1920	Definition new parameters & noise sources
makedefs	10	Entry for new source file nevalsrc2.c
nevalsrc2.c	New source file	New function for correlated noise source definition